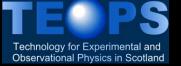
Lessons learned from SCUBA-2 for future cryogenic instrumentation in space

Adam Woodcraft http://woodcraft.lowtemp.org SUPA, University of Edinburgh/ATC



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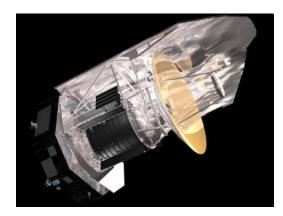
SCUBA

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- Building good sub-Kelvin (< 1 K) instruments is hard
 - Building good instruments for space is hard
 - Doing both at once is very hard!

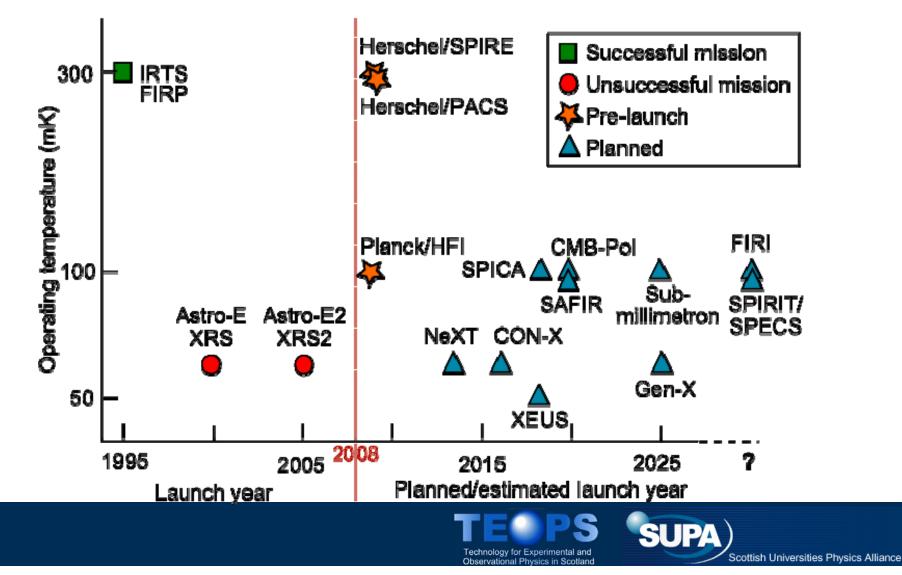








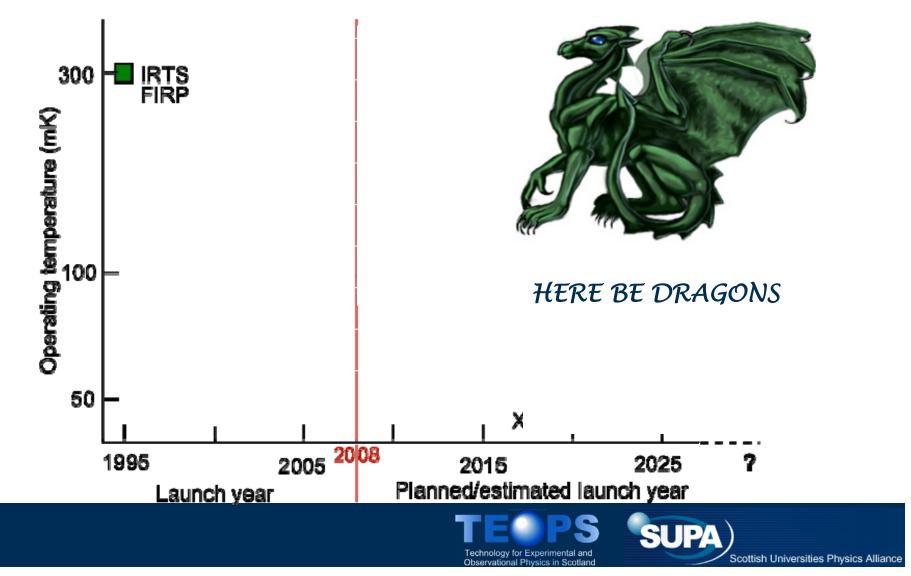
• But there are many planned missions which will require this





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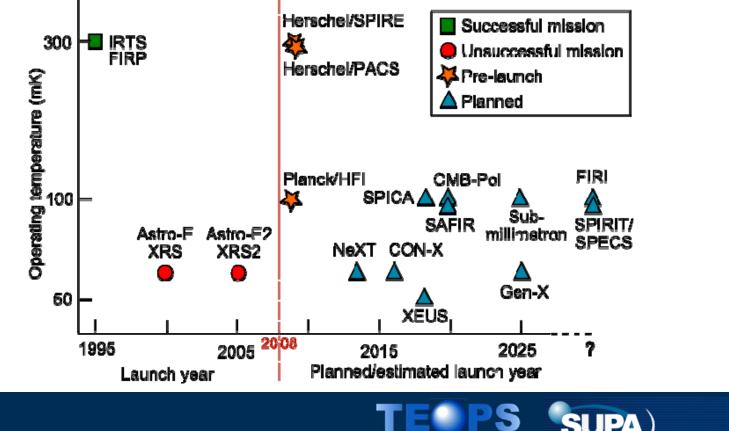
Current experience is somewhat limited





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- Probably not all of these will fly
 - But (barring breakthrough in technology), future
 - FIR/Sub-mm and X-ray missions will need ULT detectors
 - Some missions already in study phase



Technology for Experimental and

Observational Physics in Scotland



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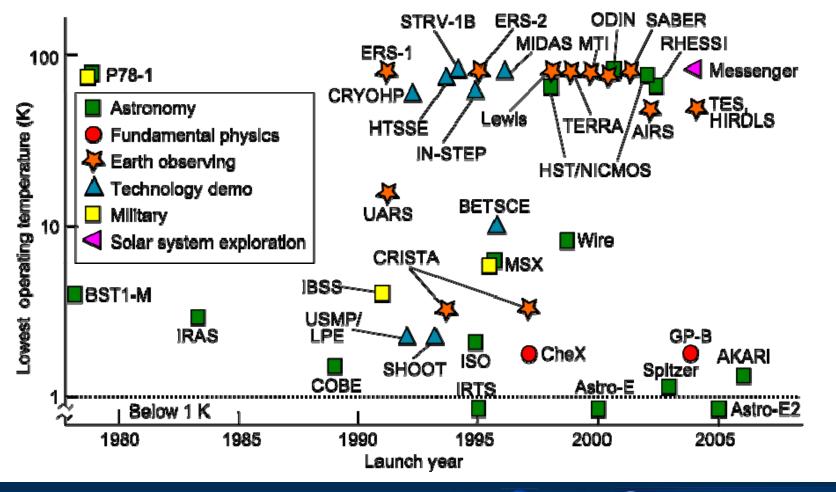
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- ULT systems require full cooling chain
 - Experience at higher temperatures extensive





- BUT:
 - Future ULT missions likely to be more demanding than those already built
 - Need to look to experience on the ground
- SCUBA-2: most complex ULT astronomical instrument ever built?
 - Future space missions likely to have similar complexity but with severe mass, power, volume etc. constraints
 - Even as a ground-based instrument, SCUBA-2 was not straightforward
 - So what did we learn from SCUBA-2?







• A wide-field imaging camera with up to 1000× the mapping capability of SCUBA

- Capable of carrying out large-scale surveys of the submillimeter sky
- Ultra-deep imaging to the (extragalactic) confusion limit
- Polarimetry and medium resolution spectroscopy also available



SCUBA-2



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SCUBA-2



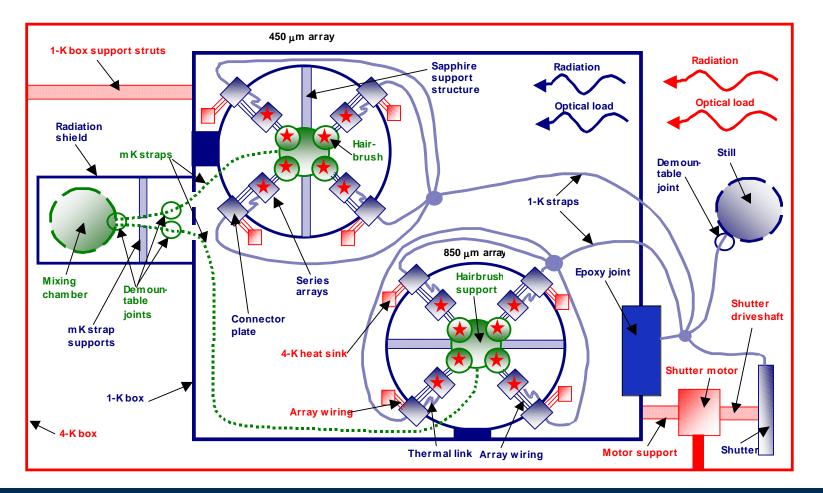
- SCUBA-2
 - Two focal planes each made from 4 subarrays massing ~ 10 kg each
 - Operate from heat sink < 50 mK, ~ 1 m from cooling source (dilution fridge)
 - Arrays have to be individually removable
 - Have to support arrays rigidly with low heat leak onto mK stage
 - Cryocooler operation





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Most challenging part of the thermal design

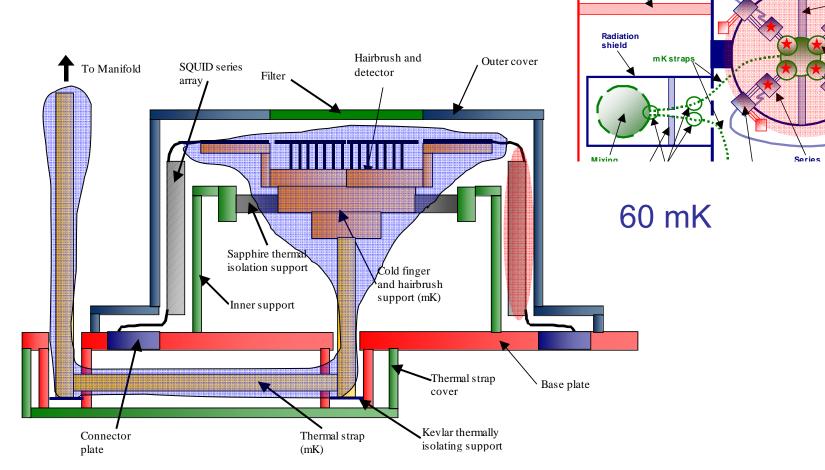




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Detector unit

SCUBA-2 - 1-K box





1-K box support struts

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brush

Sapphire support structur

> 850 μr Haiı

450 μm array





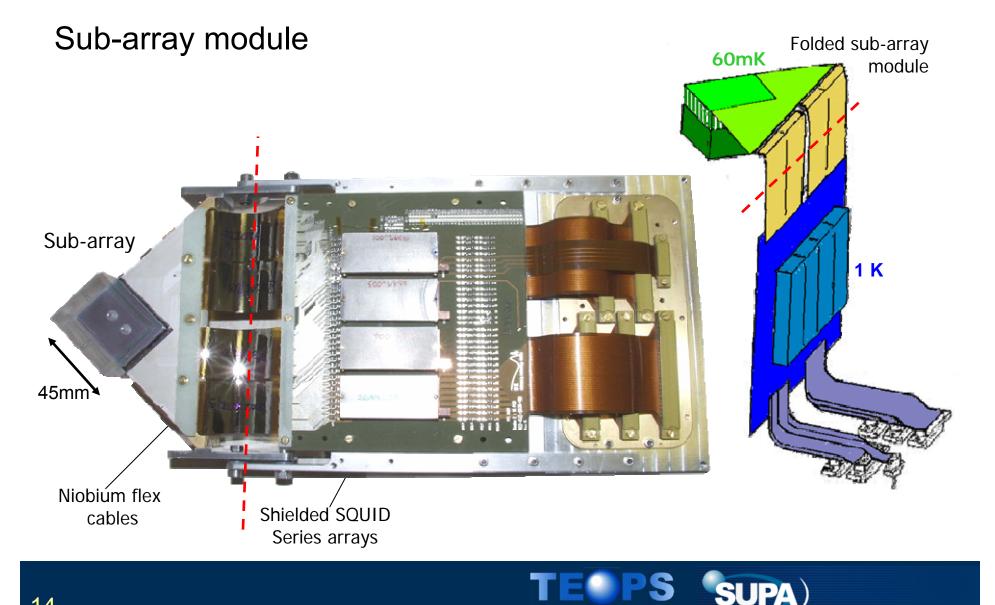
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Sub-array module Folded sub-array 60mK module Hairbrush and Outer cover To Manifold SQUID series detector Filter array 1 K Sapphire thermal isolation support Cold finger and hairbrush support (mK) Inner support Thermal strap Base plate cover Kevlar thermally Connector Thermal strap isolating support plate (mK)



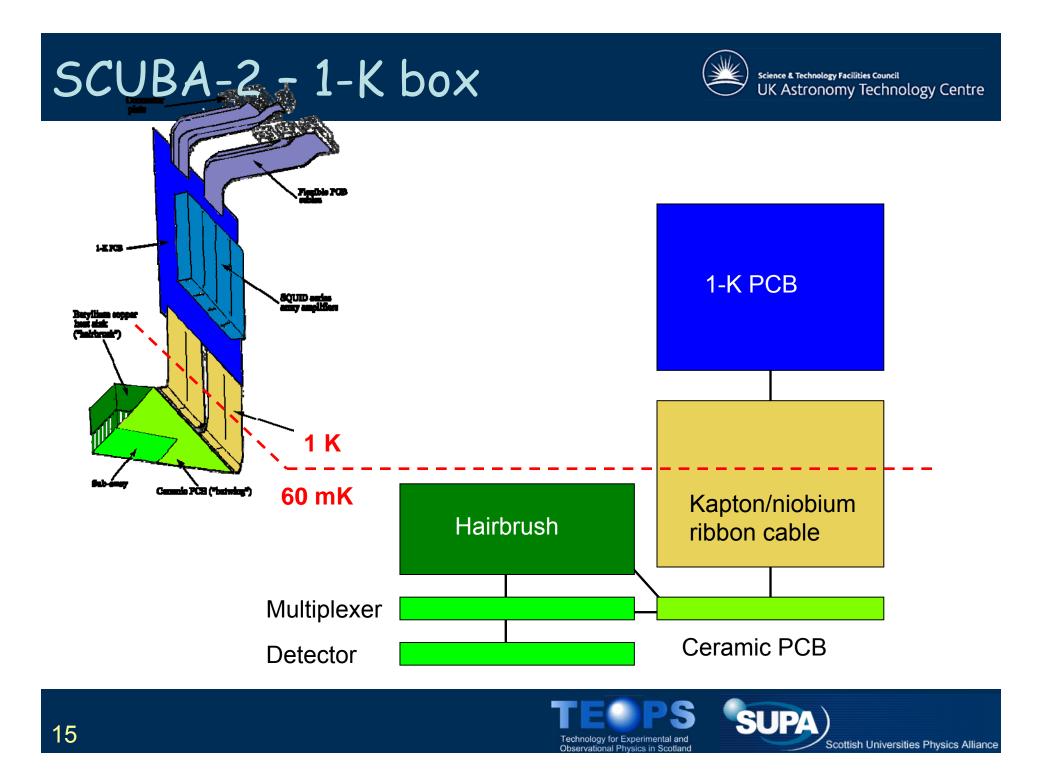


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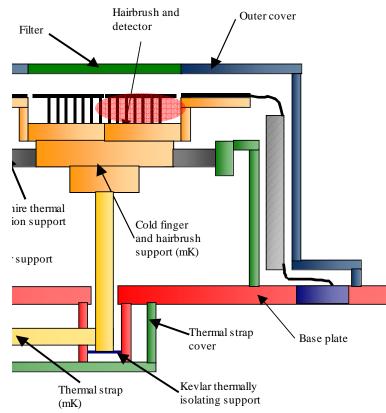


SCUBA-2 - hairbrush



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Provides heat sinking and mechanical support to detectors without breaking them due to differential thermal contraction Made from high conductivity beryllium copper alloy







SCUBA-2 - hairbrush



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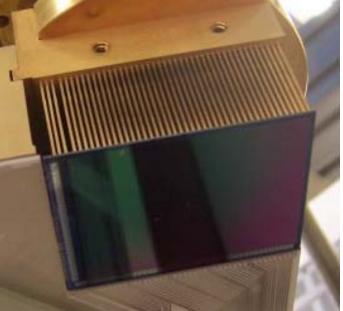
Glueing has to be uniform, musn't bridge the tines Thermal conduction has to be good enough Have to get it right first time – detector arrays are very valuable

Lengthy test programme, making and testing samples Solution: desktop robot deposits metered blob of epoxy on

each tine Haven't lost an array yet!

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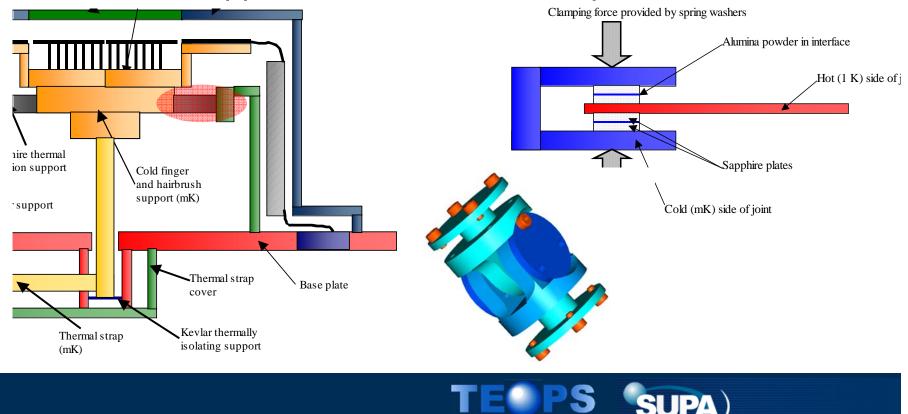
SCUBA-2 - sapphire support

Need to support arrays rigidly with low heat leak Wanted to avoid Kevlar (creep and catastrophic failure possible)

Solution: "sapphire interface" support: 2.5 μ W heat leak from 1 K to 100 mK - sapphire discs with alumina powder between

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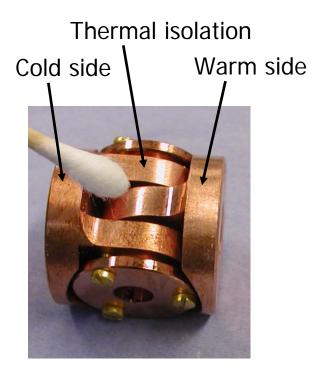


Technology for Experimental and

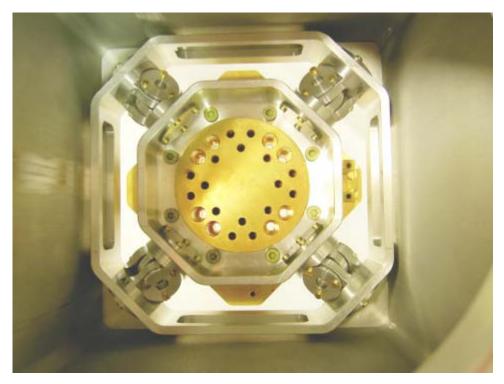
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SCUBA-2 - sapphire support Science & Technology Facilities Council UK Astronomy Technology Centre

Test joint:



Finished isolation support



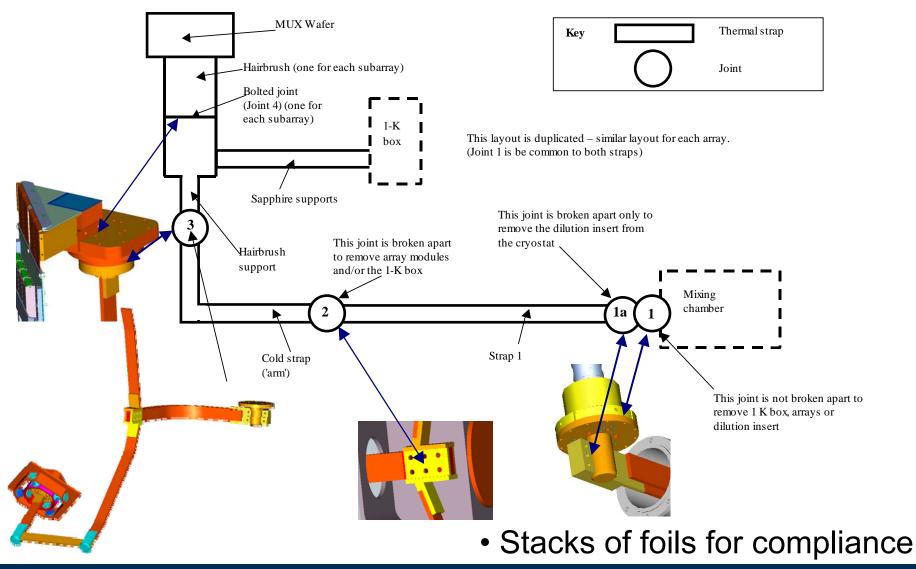
$2.5\ \mu\text{W}$ heat leak from 1 K to 100 mK Used in Clover

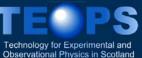


Strap system



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Material properties



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- Lack of information on material properties was a problem
 - Not unique to SCUBA-2, but more serious issue than for small instruments
 - Couldn't always use tried and tested materials
 - Had to carry out tests
 - Even with well known materials, have to worry about sample variation

Worse, G10 is a specification on *electrical* properties, not thermal or mechanical, or even the composition! Using G10 is therefore risky





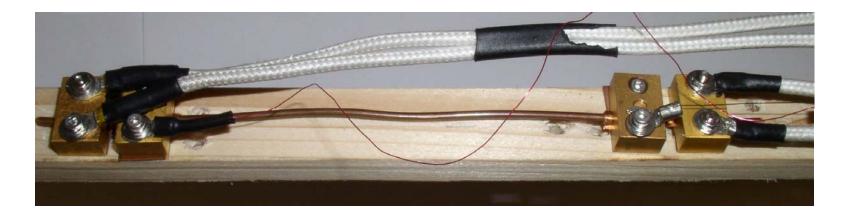
Material properties



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It is *essential* to test conductivity of same materials that will be used, with the same treatement (e.g. annealing) SCUBA-2 required considerable test campaign

Fortunately, this can be done electrically (Wiedemann-Franz law) for metals



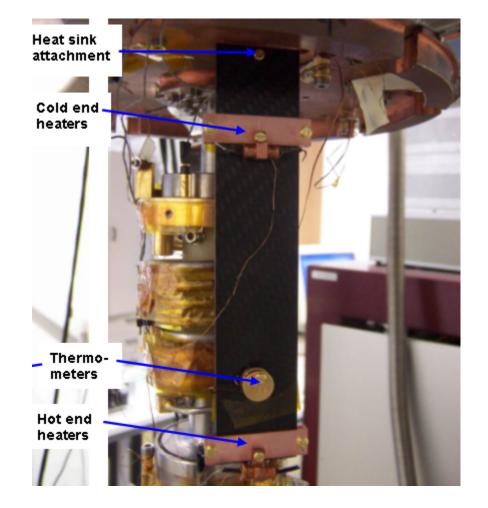


Material properties



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The 1-K box is supported from the 4-K shield with CFRP Properties are somewhat variable depending on the exact composition, and possibly from lot to lot We therefore measured the conductivity of samples from the material used





Joints



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- Joints are even harder than getting the straps right
- Fixed joints can be made by electron beam welding, giving near bulk properties
 - IF the welding is done properly...



Joints

Removable joints are the hardest. Not very well understood.

Little data to enable accurate modelling; depends on many variables.

Gold plating required to avoid oxide layer

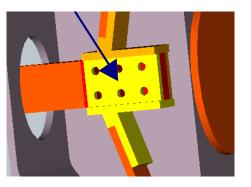
Need to use high pressure (multiple bolts, high torque). Do **NOT** use grease!

Performance not necessarily repeatable

Again, electrical tests are very useful

Every joint must perform sufficiently well! A single poor joint can destroy the usefullness of the entire cooling chain





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The 1-K radiation shield is made from an aluminium alloy to minimise weight.

This gives us two problems:

- 1) The thermal conductivity of aluminium alloys is relatively poor
- 2) It is hard to make good contact to aluminium because of the tenacious oxide layer
 - Gold plating aluminium is difficult, and would be even harder for such a large structure





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A system of 1-K straps ensures good heat sinking to components

Straps are similar, and have similar issues, to mK straps

- Requirements are less demanding
- But we have rather more straps and contacts





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We still need to make good thermal contact to the box itself to cool it and maintain its temperature

- Requirement: temperature < 1.5 K to minimize radiation
- Wiring heat sinks must be < 1.1 K to minimize heat leaks
- Hot end of sapphire supports must also be < 1.1 K

To avoid poor conductance due to the oxide layer on aluminium, we forego metal to metal contact and use a large area epoxy joint to a copper plate. A bolted joint can then be made to this plate

- Trade large microscopic contact area for poorly conducting intermediate layer
- Worked well on SPIRE





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In the first test, the instrument cooled down below required temperature, and more quickly than required.

So we did something right!







What did we do right?



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- More generally....
- Thermal design treated as integral; large amount of effort (not something you bolt on afterwards)
- Project team *experienced*, and *at this temperature range* (100 mK is not 2 K!)
 - Thermal design not always treated as seriously as it should be?
- Experience from outside astronomy on review boards
- Detailed thermal model updated in parallel with mechanical design
- Subsystems tested before finalising design where possible; otherwise large margins used

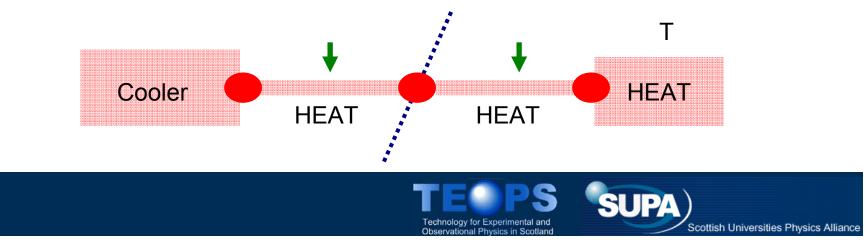




Subsystems



- Problems with splitting cryogenic systems into separate subsystems
 - Example: far end has maximum tolerable T
 - Must divide into contribution from each subsystem
 - Each subsystem needs power budget. Cooler temperature depends on power
 - BUT we have to set these budgets *before* detailed design, yet we don't know appropriate values at this point
 - We've now turned a simple system with one requirement
 (T) into something much more complex

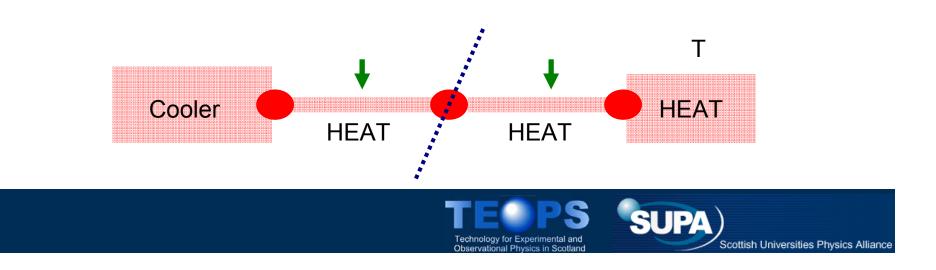


Subsystems

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- Probably can't avoid splitting into subsystems. But can:
 - Define carefully, basing not entirely on mechanical considerations
 - Have strong oversight of overall thermal design
 - Be ready to adjust requirements where necessary



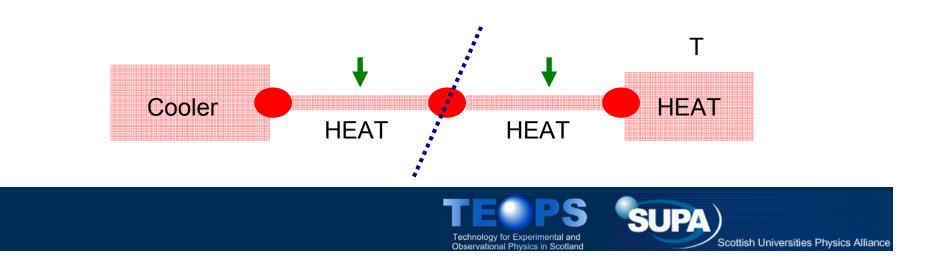
Subsystems



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From a mechanical point of view, a bolted joint in a strap is an obvious interface

- But from a thermal point of view this is a subsystem, which should be designed and tested in one piece
- (And whose thermal budget does the temperature drop across the interface come out of?)



What did we do wrong?



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- Decoupled thermal and mechanical design too much after initial design
 - Elegant thermal design was corrupted piece by piece to meet mechanical requirements
- Didn't have time to test all sub-components
 - Had to overengineer
 - Unlikely to be an option for ULT space missions!



What did we have to do wron

- Limited design by concentrating on materials which have already been measured
- Stopped tests as soon as we had a good enough solution for SCUBA-2
 - With further testing could have developed more generic solutions and more understanding of principles
- These are near universal problems
 - Something needs to be done!



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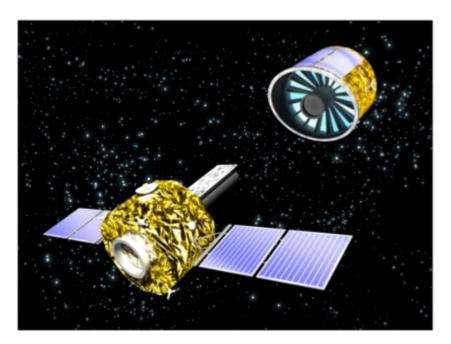
Conclusions

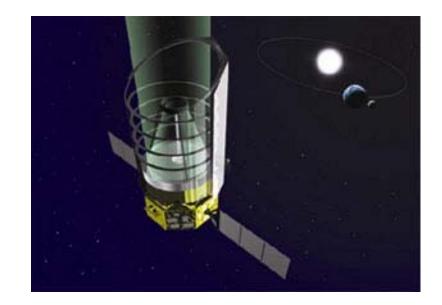


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• There will be great challenges ahead for ultra-low temperature cryogenic space missions

• We *must* learn from experience (good and bad) with current ground and space instruments!











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• "A little knowledge is a dangerous thing"

 "It's not what we don't know that's the problem, it's what we know that ain't so"

