

Understanding the Herschel-SPIRE bolometers

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Credits

Hien Nguyen, JPL James Bock, JPL Matt Griffin, Cardiff Bernhard Schultz, IPAC

Bruce Sibthorpe, Edinburgh Bruce Swinyard, RAL

....plus many many more....



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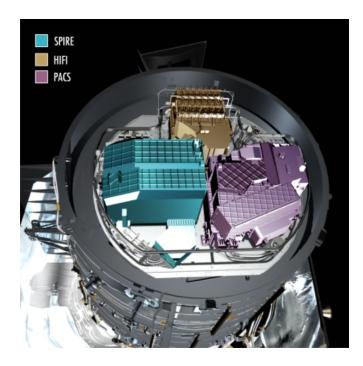
Introduction





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SPIRE: the Spectral andPhotometric Imaging ReceiverOne of three instruments on theHerschel Space Observatory



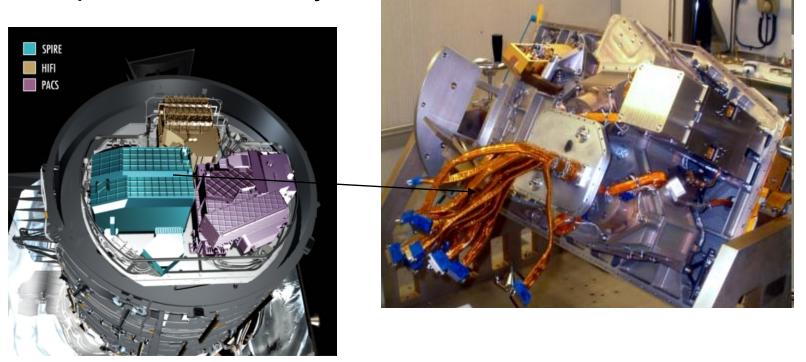






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SPIRE: the Spectral andPhotometric Imaging ReceiverOne of three instruments on theHerschel Space Observatory



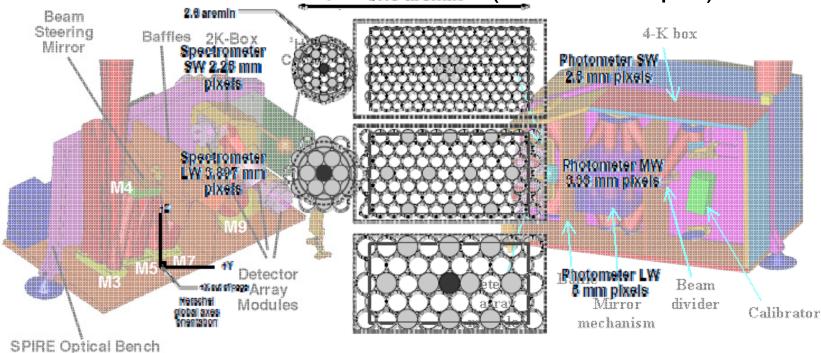




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SPIRE contains five bolometer arrays

Three form a three-band imaging photometer (centre wavelengths approx. 250, 350 and 500 µm).6 arcmin (200 to 670 µm)

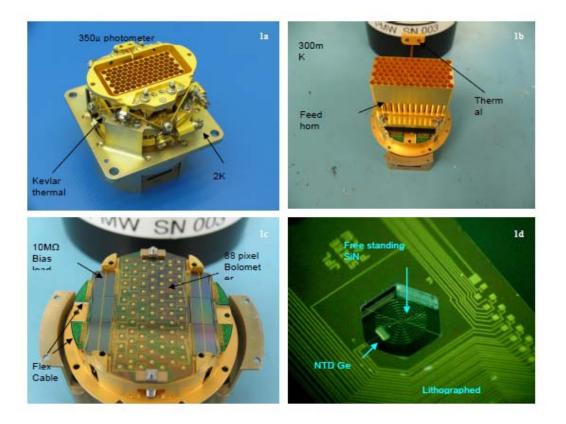


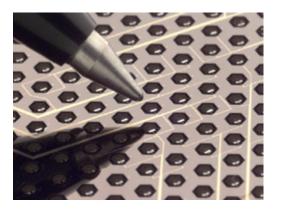




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Arrays: feedhorn coupled, NTD germanium thermistors, silicon nitride spiderweb bolometers







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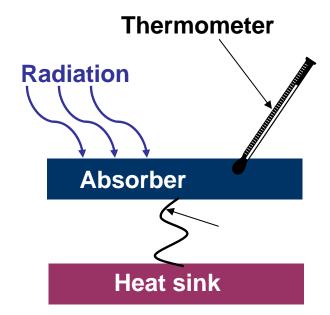
Measurements





Bolometers are very simple devices Operation is based upon well understood straightforward physics Can describe behaviour with a simple model

...in principle



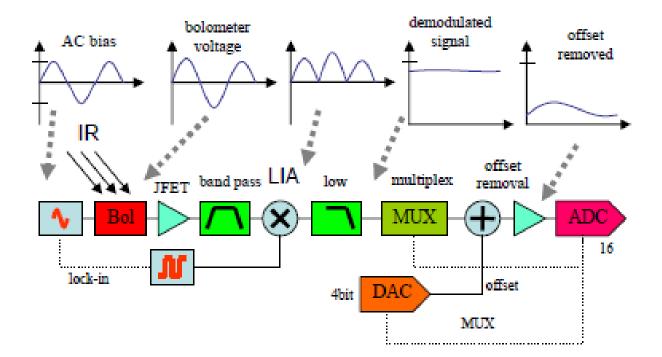
Possibly in practise....but we have to prove it! Many possible complications.



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Flight readout system is not simple! (for very good reasons)



Have to worry about effects such as cable capacitance, JFET gains varying with bias frequency...





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Load curves measured at JPL

- On each array individually
- DC bias
- Dark
- Optically loaded
- Pixels fully characterised

Load curves measured at RAL

- On arrays in the instrument
- AC bias (flight electronics)
- Dark (bolometers blanked off)
- Optically loaded (blackbody 6 to 15 K)







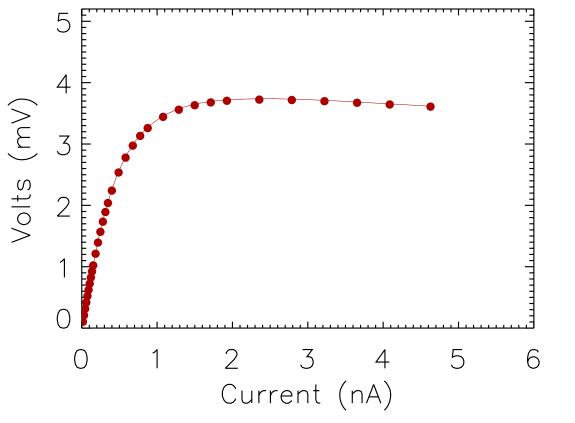




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What is a load curve?

Just a measurement of bolometer (thermistor) voltage as a function of bias current





Why measure load curves?

• Give us the information we need to fully characterise the (static) properties of the bolometers

- Can predict voltage for given
 - bias current
 - heat sink temperature
 - optical power
- So we can simulate their behaviour under different conditions
- Detect if changes have occurred post-launch
- Improve/simplify calibration





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Calibration can be done entirely empirically

- As usual for bolometer instruments
- (But empirical pipeline makes assumptions on bolometer behaviour; stability, ideal behaviour)

But if we can accurately model the detectors we can

- Check and possibly improve empirical corrections for
 - non-linearity
 - heat sink temperature variations
 - change in bias current/frequency
- Possibly even use the model directly for calibration

Information on detector/readout stability tells us how often (if at all) we need to recalibrate (PCAL/external source)







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Goals:

We would like to know:

- That the behaviour of the bolometers and readouts is self-consistent and stable with time
- Ideally, that the bolometers can be modelled with a simple model
 - What parameters to use with the model

We can try to show both using load curve measurements





Why are the *instrument level* measurements (load curves) so useful?

- •Tell us about performance of the arrays
 - In the instrument itself
- Give series of measurements over longer time period

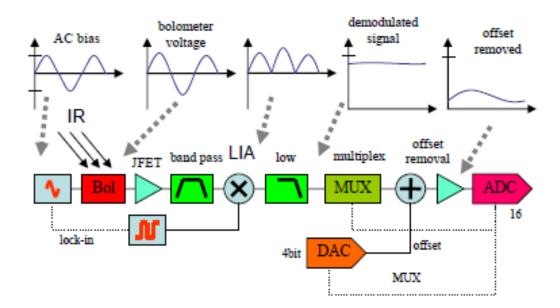
• Characterisation of pixels while in the instrument gives us direct information on behaviour in flight

- Don't have to allow for differences between readout system used in array level test (e.g. varying JFET gains, AC vs DC bias)
- But: readouts not optimised for this task





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Flight readout system is optimised for carrying out astronomical observations, not load curves

- Low noise (therefore AC bias)
- Sit at fixed bias value, measure small changes in bolometer voltage





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Consistency



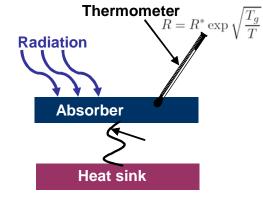
Consistency

First step in characterisation: work out R(T) for each bolometer

- Take series of load curves at different heat sink temperatures
- Take resistance in limit of zero bias
- This only works in the absence of optical radiation

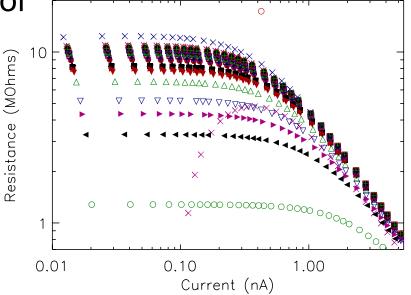
$$R = R^* \exp \sqrt{\frac{T_g}{T}}$$

• Need to automate: SPIRE has a lot of pixels!



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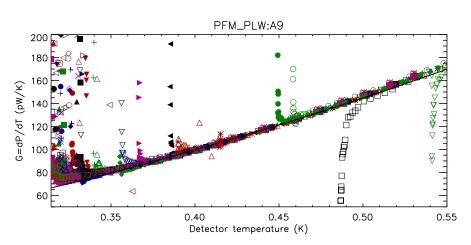
Consistency

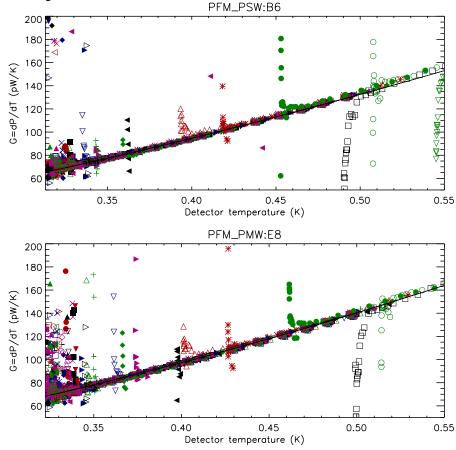


Now we can look at consistency without further analysis

- Plot G=dP/dT can compare any load curve
- Measurements over:
 - ~ 4 months
 - two cooldowns
 - different bias frequencies
- Excellent agreement!

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200

180

160

100

80

60

0.35

0.40

G=dP/dT (pW/K)

140 120

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200 🛒

160 G=dP/dT (pW/K) 140 120 100 80

₩

0.55

Consistency

Therefore:

- Bolometers and readouts are stable
- We have suitably allowed for AC effects

PFM_PLW:A9

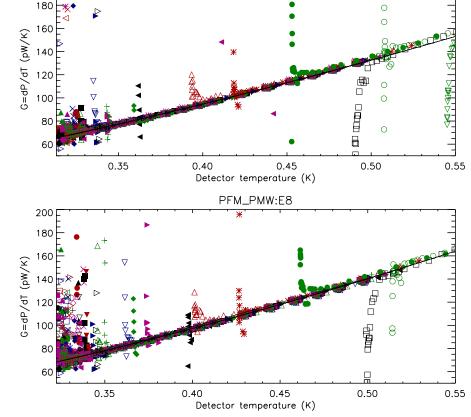
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0.45

Detector temperature (K)

0.50







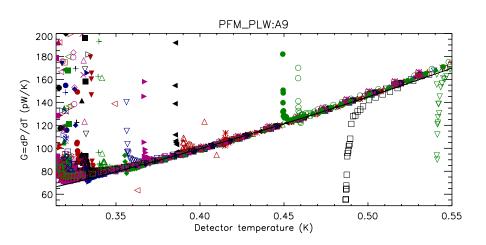
PFM_PSW:B6



Consistency

Therefore:

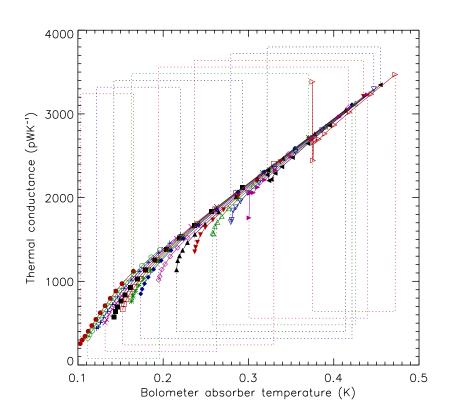
- Bolometers and readouts are stable
- We have suitably allowed for AC effects
- Bolometer resistance depends on temperature alone



Unlike for this non-SPIRE (100 mK) bolometer, showing E-field(?) effects

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Thermal model

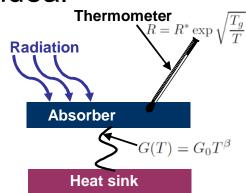


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We can do further analysis with the thermal ("ideal bolometer") model

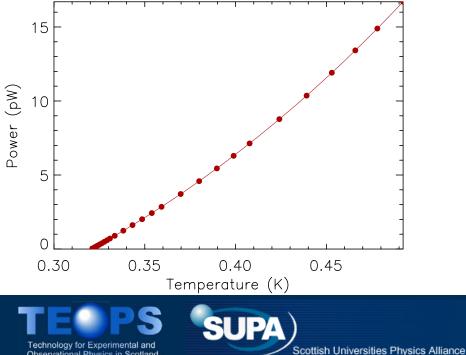
 $G(T) = G_0 T^{\beta}$

Having obtained R(T), we can get G(T)from any load curve by doing a non-linear fit to power vs temperature



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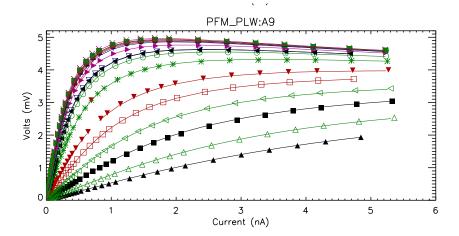


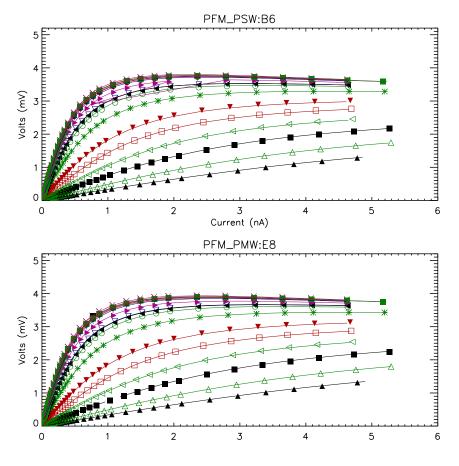
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Results (plotted as voltage vs current)

- •Turnover due to electrothermal feedback
- Very good fits
- These are *not* individual fits to each load curve; parameters taken from one load curve only

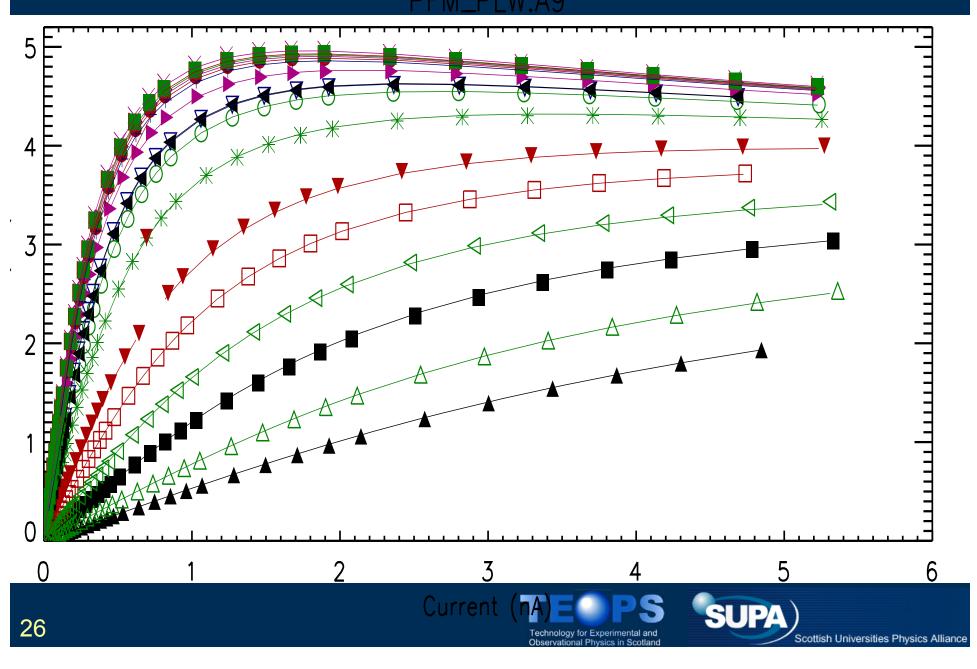
• So we can predict bolometer performance well





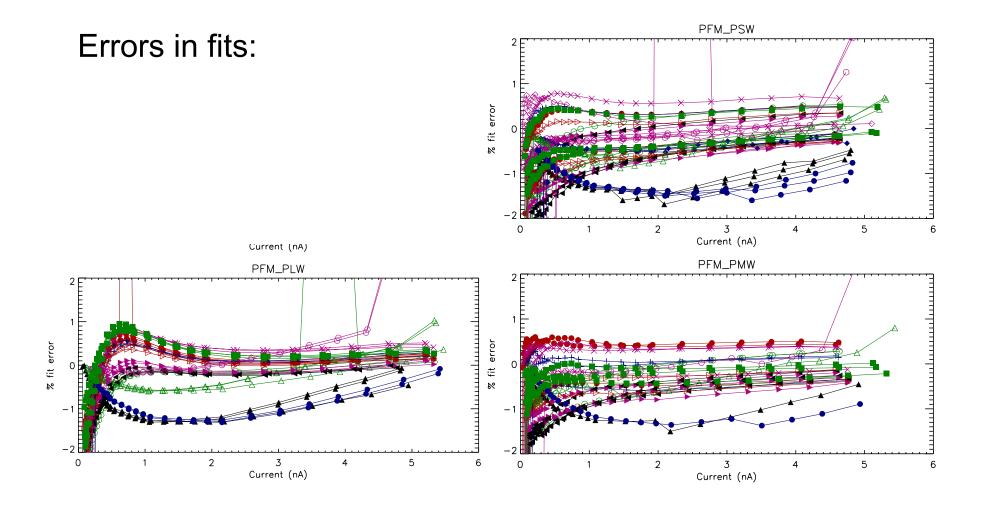


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Actually; we already know this should work:

These plots showed that PFM_PSW:B6 200 🛒 $G(T) = G_0 T^\beta$ 180 160 G=dP/dT (pW/K) is a good assumption 140 120 (black lines show model fits) 100 80 8 60 0.35 0.40 0.45 0.50 0.55 Detector temperature (K) PFM_PLW:A9 PFM_PMW:E8 200 200 180 180 160 G=dP/dT (pW/K) G=dP/dT (pW/K) f R 80 60 0.35 0.40 0.50 0.55 0.45 0.35 0.40 0.45 0.50 0.55 Detector temperature (K) Detector temperature (K)

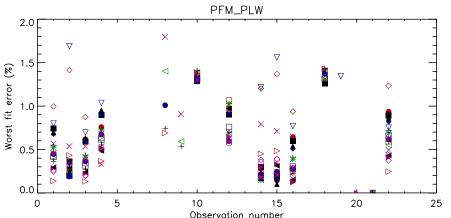


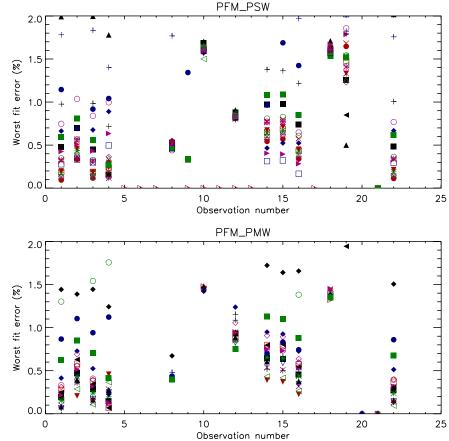


But so far I've only shown results for three bolometers – "typical results".

• How typical are they?

These plots show the maximum errors in fits to all blanked load curves for 75 bolometers









Here is the same thing for *all* bolometers for a single simultaneous measurement

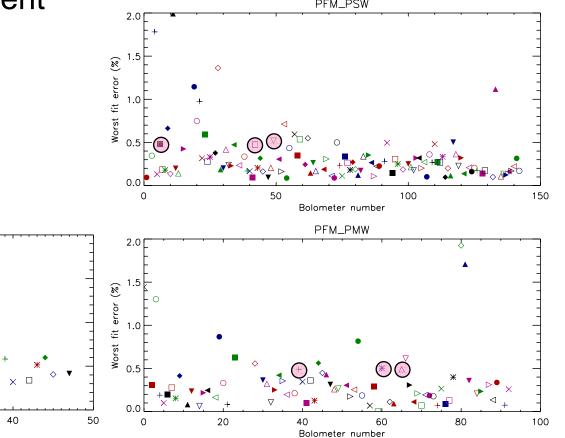
My "typical" results highlighted here; worst case apart from outliers

PFM_PLW

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Bolometer number

30





2.0

1.5

0.5

0.0

0

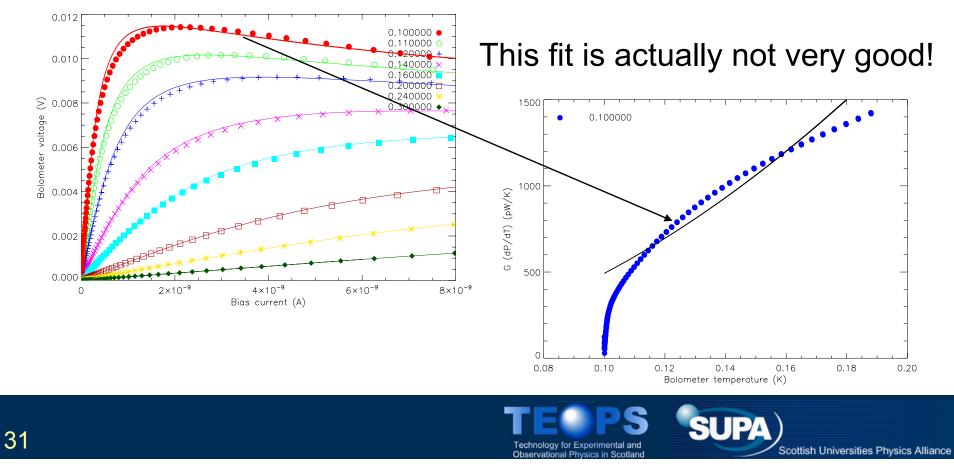
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Worst fit error (%)



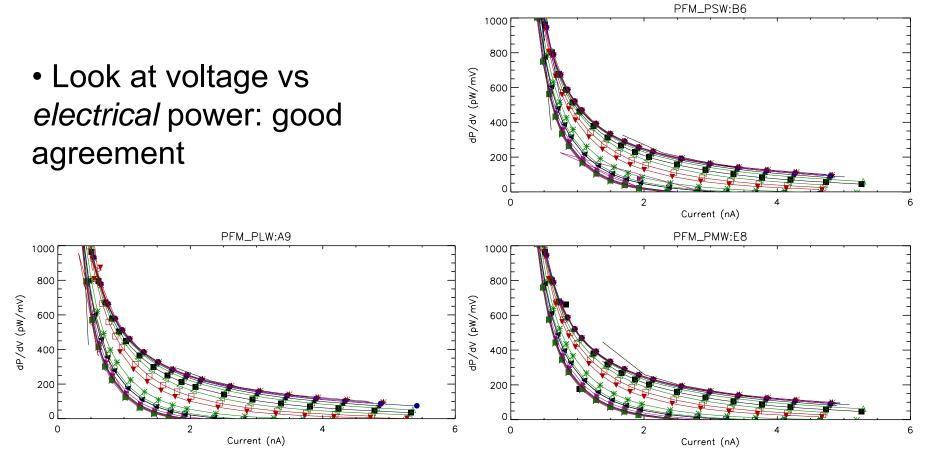
So the thermal model works very well.

- But just because the fits look good as voltage vs current doesn't mean all is well.
- Case study (for a 100 mK bolometer) below:





We know the model fits G(T) nicely here, but we really want to measure changes in optical power







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How about optical power?

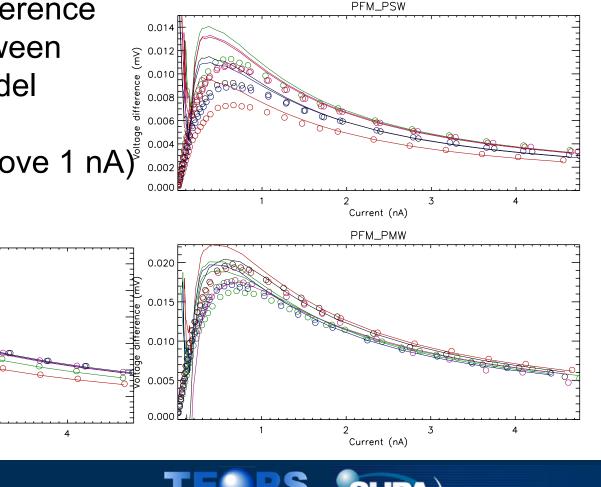
- Take two load curves with similar optical power
- Compare voltage difference at fixed bias point between measurement and model
- Good agreement (above 1 nA) for ΔV for this ΔP

2

Current (nA)

3

PFM_PLW



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0.030E

0.025

0.020

0.015

0.005

0.000

1

difference (mV)

voltage



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So the model works well.

We should be able to use it to allow for

- Effect of variations in heat sink temperature
- Non-linear response
- Changes in operating bias current and/or frequency without any empirical terms





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Conclusions



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Conclusions



- •The bolometers and readout systems are extremely stable
- We understand how to correct for AC bias effects in order to characterise the detectors using measurements in the instrument
- A simple bolometer model using parameters from this characterisation fits the measurements extremely well
- We can therefore predict the bolometer behaviour under difference conditions in flight
- Work on using the model to obtain absolute (absorbed) power measurements from the bolometers with no external calibration is showing promising results

